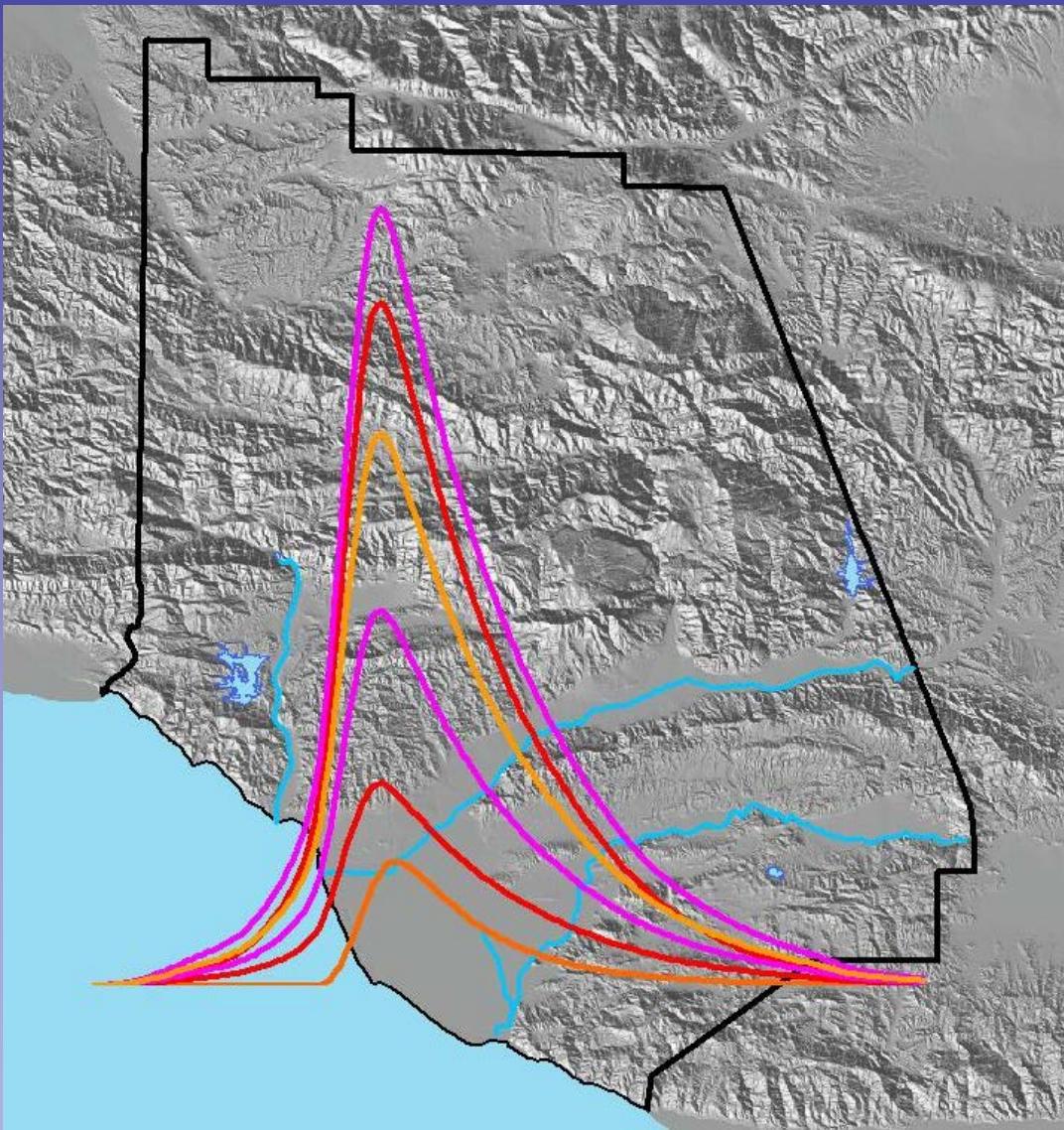


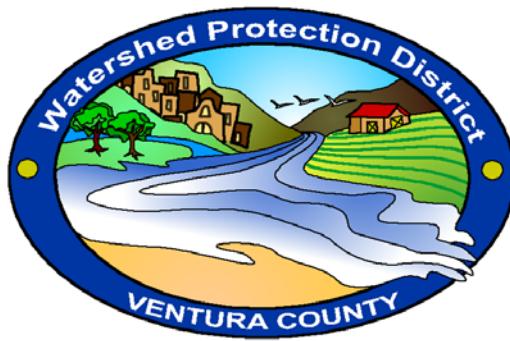
SANTA CLARA RIVER FRANKLIN-WASON-BROWN-CLARK- SUDDEN WATERSHEDS HSPF DESIGN STORM MODELING

Final Addendum I



December 2013
Hydrology Section
Watershed Resources and Technology Division
Ventura County Watershed Protection District

Saticoy Area Design Storm Modeling



Ventura County

Watershed Protection District

Hydrology Section

Project 12512

District Director: Tully Clifford

Engineering Manager: Bruce Rindahl

Author: Mark Bandurraga

Reviewers: Zia Hosseinipour, Yunsheng Su

EXECUTIVE SUMMARY

This report documents the work done by Kasraie Consulting (KC) for the Ventura County Watershed Protection District (VCWPD) in adapting the design hydrology for the Saticoy area watersheds of Franklin, Brown, Wason, Clark, and Sudden Barrancas. The design storm peaks and hydrographs were used for two-dimensional floodplain model of the watershed using FLO-2D. The design hydrology was based on the calibrated Santa Clara HSPF Model (Aqua Terra 2009). The main report (VCWPD, 2013) presented results for the regional-scale subareas included in the HSPF model.

KC prepared numerous additional hydrographs based on the regional model results for use in the FLO-2D model. The additional hydrographs were required to minimize the effects of using a hydrograph-based hydrology approach on the FLO-2D model results. The use of numerous hydrographs was necessary to approximate the spatial distribution of runoff that occurs in a design storm.

KC first subdivided the HSPF watersheds shown in Figure 1 into 177 smaller subareas as shown in Figure 2. This includes additional subareas outside of the original HSPF watersheds. They then took the HSPF 100-yr output hydrographs and pro-rated them by area based on the FLO-2D subareas. Next, they applied the design storm ratios supplied in the main report to convert the 100-yr hydrographs to other design storm frequencies for their modeling efforts. For storm events different from the 100-yr storm, hydrographs were converted based on land use designation as described in the report.

The District then reviewed the results and concluded that the FLO-2D hydrographs were consistent with the HSPF results and were suitable for use in the Saticoy area FLO-2D modeling effort.

TABLE OF CONTENTS

| | |
|---|----|
| EXECUTIVE SUMMARY | ii |
| 1. INTRODUCTION | 1 |
| 2. FLO-2D HYDROGRAPHS | 1 |
| 2.1. Areas Outside of the HSPF Model..... | 1 |
| Figure 1 - 2013 HSPF Subareas and Reach Numbers..... | 2 |
| Figure 2 - FLO-2D Subareas | 1 |
| Figure 3 - HSPF Areas and Additional FLO-2D Subareas..... | 2 |
| Figure 4 - FLO-2D Subarea Land Use (U=Urban, A=Ag or Undev.)..... | 3 |
| 2.2. Design Storm Ratio Application | 4 |
| 2.3. FLO-2D Peak Flows | 4 |
| 3. SUMMARY AND CONCLUSIONS..... | 4 |
| Table 1 - HSPF Subarea 886 Pro-Rated FLO-2D Results..... | 5 |
| Table 2 - HSPF and FLO-2D Comparison Table | 6 |
| 4. REFERENCES | 7 |
| 5. FILES..... | 7 |
| 6. APPENDIX A – FLO-2D HYDROGRAPH DATA | 8 |

1. INTRODUCTION

This report documents the work done by Kasraie Consulting (KC) for the Ventura County Watershed Protection District (VCWPD) in adapting the design hydrology for the Saticoy area watersheds of Franklin, Brown, Wason, Clark, and Sudden Barrancas. The design hydrology was provided by the calibrated Santa Clara HSPF Model (Aqua Terra 2009). The model was used to provide the design storm peaks and hydrographs for two-dimensional floodplain modeling using FLO-2D. The main report (VCWPD, 2013) presented results for the regional-scale subareas included in the HSPF model.

KC prepared numerous additional hydrographs based on the regional model results for use in the FLO-2D model. The additional hydrographs were required to minimize the effects of using a hydrograph-based hydrology approach on the FLO-2D model results. The use of numerous hydrographs was necessary to better approximate the spatial distribution of runoff that occurs in a design storm and account for the timing of flow throughout the model domain more accurately.

2. FLO-2D HYDROGRAPHS

KC first subdivided the HSPF watersheds shown in Figure 1 into 177 smaller subareas as shown in Figure 2 and created 177 concentration points throughout the study area. The hydrologic concentration points were then spatially correlated to the FLO-2D grid elements. FLO-2D inflow nodes were then defined as either floodplain or channel elements in the Saticoy model.

They then took the HSPF output hydrographs and pro-rated them by area based on the FLO-2D subareas included in the 20 HSPF watersheds. This process was repeated for each of the six required storm frequencies.

The FLO-2D subarea boundaries follow the HSPF area boundaries with some minor exceptions. The FLO-2D subareas were checked by summing the areas and comparing them to the HSPF data.

2.1. Areas Outside of the HSPF Model

KC identified areas that were not included in the HSPF model that could contribute runoff to the developed areas in the FLO-2D model or that would drain directly to the SCR adjacently to the Saticoy redline channels. These areas are shown in Figure 3. The subarea upstream of Clark Barranca pro-rated the hydrograph from HSPF area 884 to get the runoff hydrograph. The subareas to the southwest of Clark Barranca used the hydrograph from HSPF area 885 to get the pro-rated hydrographs. The subareas to south and east of Franklin-Wason Barrancas used the hydrograph for HSPF area 874 to get the pro-rated hydrographs.

Saticoy Area Design Storm Modeling

HSPF area 885 is mostly developed and so likely results in an overestimate of the peaks for the agricultural subareas to the southeast of Clark Barranca. However, these subareas drain directly to the SCR and do not affect the flooding in the redline channels that are being evaluated in the project.

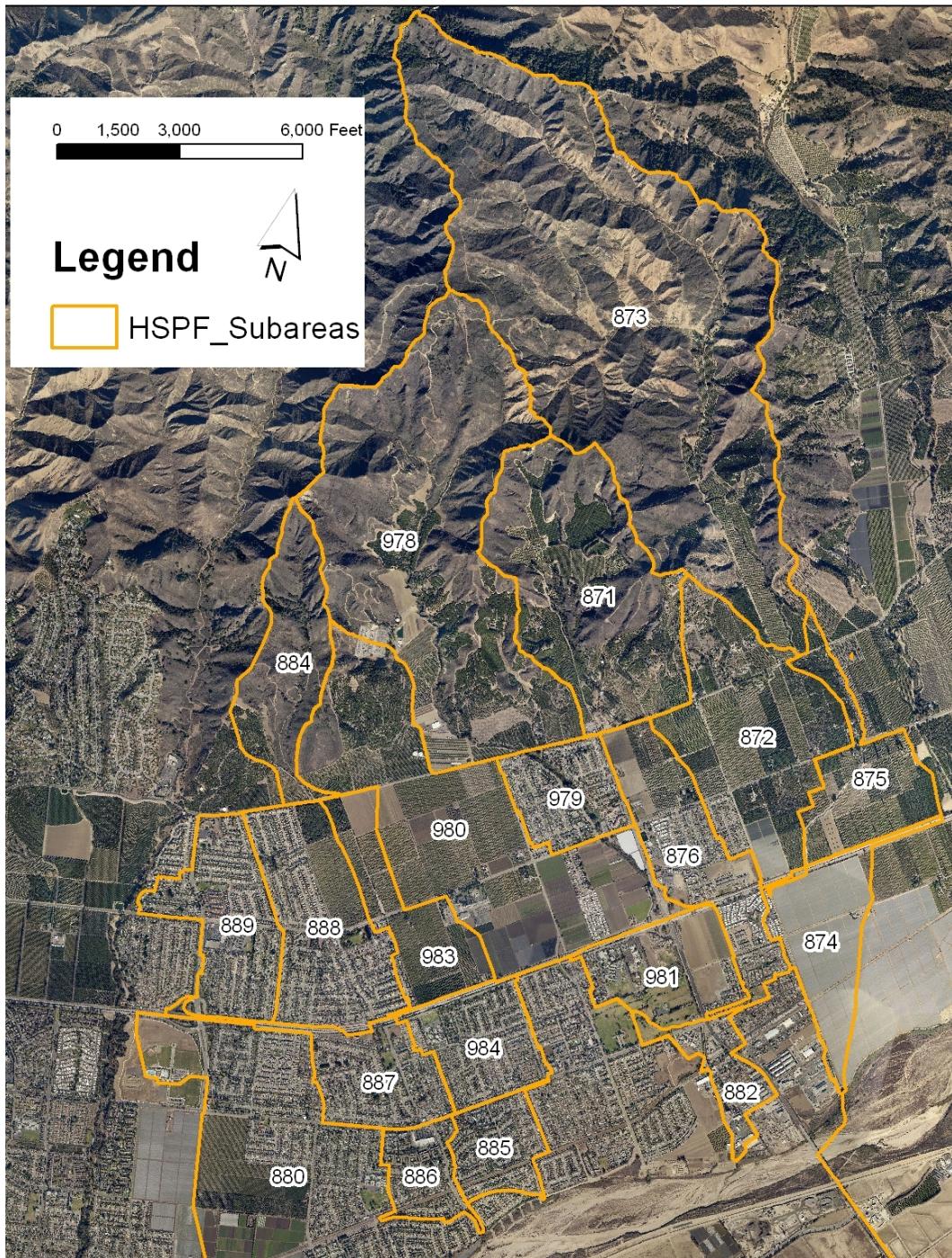


Figure 1 - 2013 HSPF Subareas and Reach Numbers

Saticoy Area Design Storm Modeling

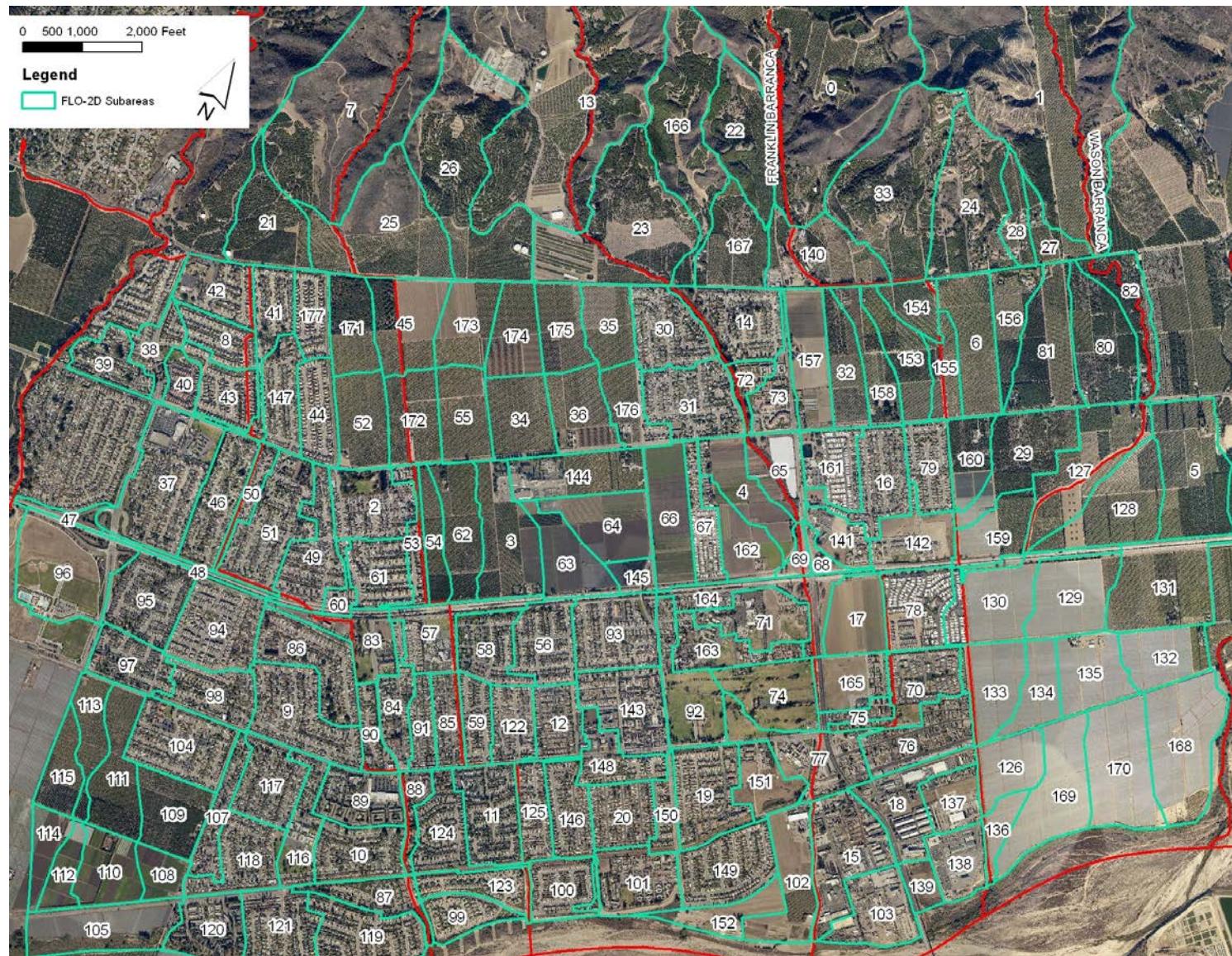


Figure 2 - FLO-2D Subareas

Saticoy Area Design Storm Modeling

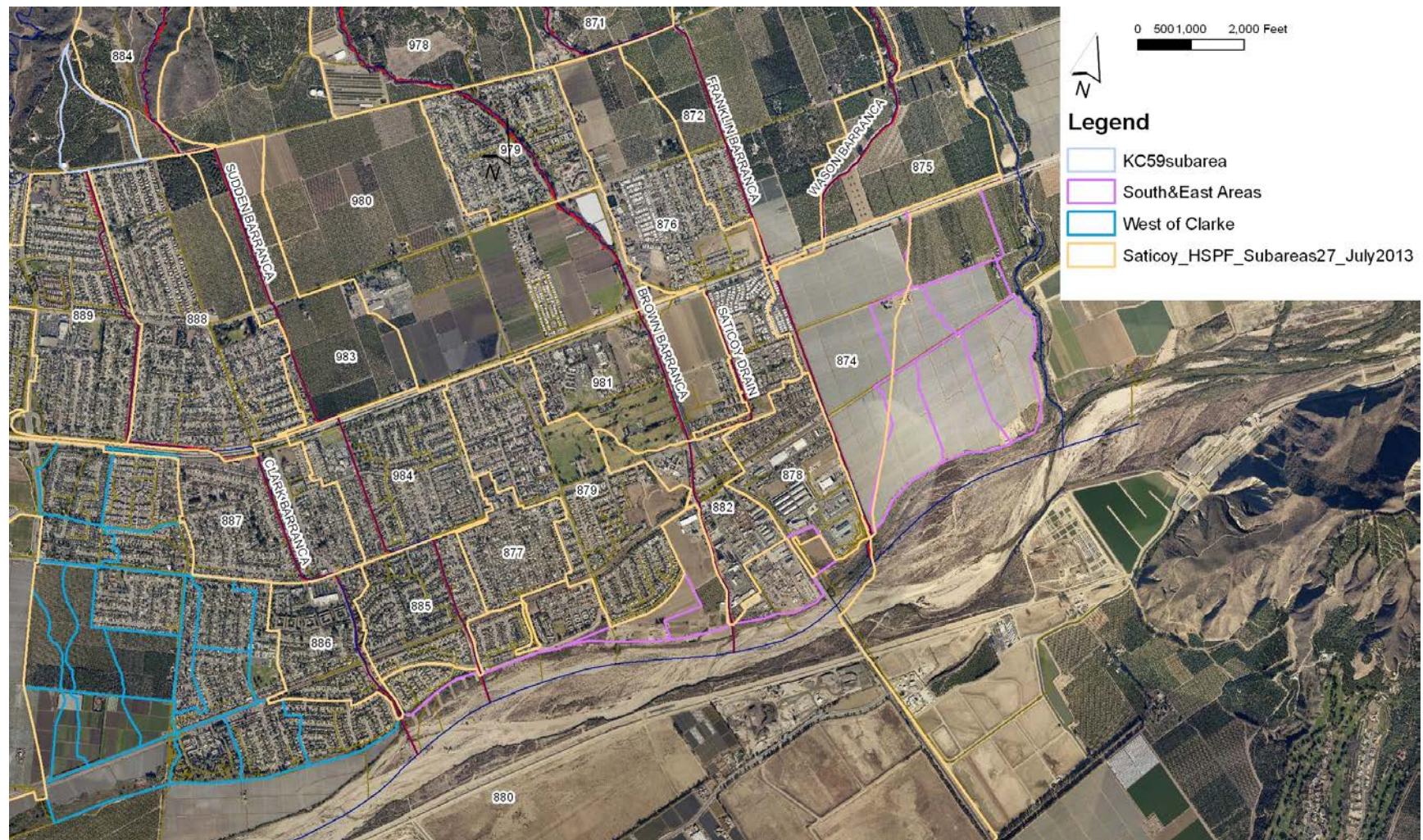


Figure 3 - HSPF Areas and Additional FLO-2D Subareas

Saticoy Area Design Storm Modeling



Figure 4 - FLO-2D Subarea Land Use (U=Urban, A=Ag or Undev.)

2.2. Design Storm Ratio Application

Figure 4 shows a map of the general land uses assigned to the FLO-2D subareas. These land uses determined if the design storm ratios from undeveloped or mixed use/developed watersheds were applied to the pro-rated HSPF hydrographs to obtain the hydrology for storm frequencies other than the 100-yr. In general, the decision to use the appropriate set of multiplier is straightforward, except for irrigated parks and one subarea in the Saticoy Drain that had two-thirds agricultural land use and about one-third high density residential land use. KC decided to use the mixed/developed ratios for these partially developed subareas and the District agrees with this engineering judgment.

KC used the average storm ratios presented in the main report (VCWPD, 2013) to convert the 100-yr hydrographs to the other required storm frequencies. Table 1 includes the design storm ratios for developed watersheds from the main report

2.3. FLO-2D Peak Flows

Table 1 shows sample pro-rating calculations for HSPF subarea 886 representing an upper portion of the developed Clark Barranca watershed. The sum of the FLO-2D peaks and volumes are slightly different than the HSPF results due to rounding used in the pro-rating calculation. Appendix A presents a summary of the peak flow and hydrograph volume data used in the FLO-2D model.

Table 2 shows a comparison of the HSPF and aggregated FLO-2D data for the entire model. The sums of the areas and peaks used in the FLO-2D model are within 2.5% or less of the HSPF regional data. The differences are due to the slight differences in area between the regional HSPF subareas and the FLO-2D areas, and also due to the rounding used in the pro-rating calculation.

The percent differences in the peak/area ratio between the HSPF and aggregate FLO-2D hydrographs is also shown in Table 2. For the most upstream subarea, the hydrograph used in the FLO-2D calculations was the routed HSPF subarea hydrograph. For any downstream subarea, the local HSPF subarea hydrograph is used in the FLO-2D calculations.

Based on the evaluation, VCWPD concluded that the hydrographs developed by KC are appropriate for use in the Saticoy FLO-2D modeling effort.

3. SUMMARY AND CONCLUSIONS

This addendum describes the work by KC to prepare numerous additional hydrographs based on the regional model results for use in the FLO-2D model. The additional hydrographs were required to minimize the effects of using a hydrograph-based hydrology approach on the FLO-2D model results. The use of numerous

Saticoy Area Design Storm Modeling

hydrographs was necessary to approximate the spatial distribution of runoff that occurs in a design storm.

KC first subdivided the HSPF watersheds shown in Figure 1 into 177 smaller subareas as shown in Figure 2. This includes additional subareas outside of the original HSPF watersheds. They then took the HSPF 100-yr output hydrographs and pro-rated them by area based on the FLO-2D subareas. Next, they applied the design storm ratios supplied in the main report to convert the hydrographs to other design storm frequencies for their modeling efforts.

The District then reviewed the results and concluded that the FLO-2D hydrographs were consistent with the HSPF results and were suitable for use in the Saticoy area FLO-2D modeling effort.

Table 1 - HSPF Subarea 886 Pro-Rated FLO-2D Results

| Channel | CLARK | | | | | |
|---------------------|-------|-------|-------|-------|------------|-------------|
| HSPF ID | 886 | | | | | |
| HSPF AREA ac. | 93.66 | | | | | |
| HSPF 100-Yr Pk cfs | 274 | | | | | |
| HSPF 100-Yr Vol. af | 53 | | | | | |
| FLO-2D ID | 10 | 87 | 88 | 89 | FLO-2D Sum | HSPF Result |
| Primary Land Use | URBAN | URBAN | URBAN | URBAN | | |
| FLO-2D Area Ac. | 31.08 | 21.82 | 11.57 | 29.19 | 93.66 | 93.66 |
| Subarea Ratios | 0.33 | 0.23 | 0.12 | 0.31 | 0.99 | 1.00 |
| Ratio 5/100-yr | 0.330 | 0.330 | 0.330 | 0.330 | - | - |
| 5-yr Peak cfs | 29.8 | 20.8 | 10.9 | 28.0 | 89.52 | 90.42 |
| 5-yr Vol af | 5.8 | 4.0 | 2.1 | 5.4 | 17.32 | 17.49 |
| Ratio 10/100-yr | 0.464 | 0.464 | 0.464 | 0.464 | - | - |
| 10-yr Peak cfs | 42.0 | 29.2 | 15.3 | 39.4 | 125.86 | 127.14 |
| 10-yr Vol af | 8.1 | 5.7 | 3.0 | 7.6 | 24.35 | 24.59 |
| Ratio 25/100-yr | 0.660 | 0.660 | 0.660 | 0.660 | - | - |
| 25-yr Peak cfs | 59.7 | 41.6 | 21.7 | 56.1 | 179.03 | 180.84 |
| 25-yr Vol af | 11.5 | 8.0 | 4.2 | 10.8 | 34.63 | 34.98 |
| Ratio 50/100-yr | 0.822 | 0.822 | 0.822 | 0.822 | - | - |
| 50-yr Peak cfs | 74.3 | 51.8 | 27.0 | 69.8 | 222.98 | 225.23 |
| 50-yr Vol af | 14.4 | 10.0 | 5.2 | 13.5 | 43.13 | 43.57 |
| Ratio 100/100-yr | 1.00 | 1.00 | 1.00 | 1.00 | - | - |
| 100-yr Peak cfs | 90.4 | 63.0 | 32.9 | 84.9 | 271.26 | 274.00 |
| 100-yr Vol af | 17.5 | 12.2 | 6.4 | 16.4 | 52.47 | 53.00 |
| Ratio 500/100-yr | 1.502 | 1.502 | 1.502 | 1.502 | - | - |
| 500-yr Peak cfs | 135.8 | 94.7 | 49.4 | 127.6 | 407.44 | 411.55 |
| 500-yr Vol af | 26.3 | 18.3 | 9.6 | 24.7 | 78.81 | 79.61 |

Table 2 - HSPF and FLO-2D Comparison Table

| Subarea Name | HSPF Reach | Area ac. | Local Subarea Peak cfs | Local Subarea Ratio cfs/ac | Routed Flow Peak cfs | Routed Flow Ratio cfs/ac | FLO-2D Area Sum ac. | FLO-2D Area Peak Sum cfs | FLO-2D cfs/ac | Cfs/ac % Change | FLO-2D Area Vol. af | FLO-2D Yield in. |
|-----------------------|------------|----------|------------------------|----------------------------|----------------------|--------------------------|---------------------|--------------------------|---------------|-----------------|---------------------|------------------|
| Upper Franklin | 871 | 539.8 | 1,460.0 | 2.70 | 1,020.0 | 1.89 | 538.9 | 1009.8 | 1.87 | 0.8% | 277.2 | 6.17 |
| Middle Franklin | 872 | 437.0 | 888.0 | 2.03 | 1,650.0 | 1.69 | 435.5 | 896.9 | 2.06 | -1.4% | 255.5 | 7.04 |
| Upper Wason | 873 | 1,665.5 | 4,560.0 | 2.74 | 2,220.0 | 1.33 | 1,662.3 | 2,220.0 | 1.34 | -0.2% | 810.0 | 5.85 |
| Middle Wason | 875 | 198.9 | 397.0 | 2.00 | 2,270.0 | 1.22 | 189.8 | 381.1 | 2.01 | -0.6% | 110.4 | 6.98 |
| Lower Franklin-Wason | 874 | 199.8 | 389.0 | 1.95 | 3,930.0 | 1.29 | 179.2 | 354.0 | 1.98 | -1.5% | 106.5 | 7.13 |
| Saticoy Op. Yard | 878 | 117.6 | 391.5 | 3.33 | NC | NC | 113.9 | 379.8 | 3.33 | -0.2% | 63.1 | 6.65 |
| Upper Brown | 978 | 1,006.0 | 2,700.0 | 2.68 | 1,590.0 | 1.58 | 1,041.7 | 1,653.6 | 1.59 | -0.4% | 532.5 | 6.13 |
| Brown Blw Foothill | 979 | 145.5 | 365.0 | 2.51 | 1,750.0 | 1.52 | 145.5 | 365.0 | 2.51 | 0.0% | 80.0 | 6.60 |
| Brown Abv 126 | 980 | 698.8 | 1,420.0 | 2.03 | 2,720.0 | 1.47 | 682.1 | 1,377.4 | 2.02 | 0.6% | 389.9 | 6.86 |
| Brown Abv Teleph. | 981 | 183.6 | 433.0 | 2.36 | 2,950.0 | 1.45 | 183.6 | 428.7 | 2.33 | 1.0% | 100.0 | 6.54 |
| Saticoy Drn at Brwn | 876 | 259.1 | 579.0 | 2.27 | 295.0 | 1.16 | 259.1 | 573.2 | 2.21 | 2.5% | 144.5 | 6.69 |
| Lower Brown | 882 | 90.5 | 265.0 | 2.93 | 3,330.0 | 1.40 | 90.5 | 265.0 | 2.93 | 0.0% | 51.0 | 6.76 |
| Saticoy Ave Drn | 879 | 232.2 | 565.8 | 2.44 | NC | NC | 232.2 | 560.1 | 2.41 | 1.0% | 125.7 | 6.50 |
| 54" RCP Nr Sudden | 877 | 76.6 | 201.9 | 2.63 | NC | NC | 76.6 | 201.9 | 2.64 | -0.1% | 43.0 | 6.74 |
| Upper Sudden | 884 | 231.7 | 623.0 | 2.69 | 372.0 | 1.61 | 219.8 | 353.4 | 1.61 | -0.1% | 107.4 | 5.86 |
| Sudden Below Foothill | 983 | 180.7 | 347.0 | 1.92 | 650.0 | 1.58 | 180.5 | 347.0 | 1.92 | -0.1% | 106.0 | 7.05 |
| Sudden Blw 126 | 984 | 165.9 | 489.0 | 2.95 | 801.0 | 1.39 | 165.9 | 489.0 | 2.95 | 0.0% | 94.0 | 6.80 |
| Lower Sudden | 885 | 109.0 | 299.0 | 2.74 | 892.0 | 1.30 | 109.0 | 299.0 | 2.74 | 0.0% | 62.0 | 6.83 |
| Upper Clark West | 889 | 232.7 | 703.0 | 3.02 | 424.0 | 1.82 | 225.2 | 681.9 | 3.03 | -0.2% | 128.0 | 6.82 |
| Upper Clark East | 888 | 309.2 | 815.0 | 2.64 | 894.0 | 1.65 | 317.1 | 815.0 | 2.57 | 2.5% | 177.0 | 6.70 |
| Clark Blw 126 | 887 | 175.4 | 535.0 | 3.05 | 1,090.0 | 1.52 | 175.8 | 540.4 | 3.07 | -0.8% | 100.0 | 6.83 |
| Lower Clark | 886 | 93.7 | 274.0 | 2.93 | 1,180.0 | 1.46 | 93.7 | 271.3 | 2.90 | 1.0% | 52.5 | 6.72 |

NC= Routed Hydrograph Not Calculated

4. REFERENCES

Aqua Terra Consultants, 2009. Hydrologic Modeling of the Santa Clara River with the U.S. EPA Hydrologic Simulation Program – FORTRAN (HSPF). November, 2009.

VCWPD, 2013. Santa Clara River Franklin-Wason-Brown-Clark-Sudden Watershed HSPF Design Storm Modeling.

5. FILES

The files associated with this project are stored in:

K:\WRT\hydrology\Watersheds\Santa Clara\SaticoyModeling

6. APPENDIX A – FLO-2D HYDROGRAPH DATA

Saticoy Area Design Storm Modeling

| ID | Channel | Area Ac. | Primary Land Use | HSPF ID | HSPF AREA ac. | Subarea Ratio | HSPF PEAK cfs | HSPF VOL af | Ratio 5/100-yr | 5-yr Peak cfs | 5-yr Vol af | Ratio 10/100-yr | 10-yr Peak cfs | 10-yr Vol af | Ratio 25/100-yr | 25-yr Peak cfs | 25-yr Vol af | Ratio 50/100-yr | 50-yr Peak cfs | 50-yr Vol af | Ratio 100/100-yr | 100-yr Peak cfs | 100-yr Vol af | Ratio 500/100-yr | 500-yr Peak cfs | 500-yr Vol af |
|----|-------------|----------|------------------|---------|---------------|---------------|---------------|-------------|----------------|---------------|-------------|-----------------|----------------|--------------|-----------------|----------------|--------------|-----------------|----------------|--------------|------------------|-----------------|---------------|------------------|-----------------|---------------|
| 0 | FRANKLIN | 347.31 | UNDEV_AG | 871 | 539.83 | 0.64 | 1020 | 280 | 0.144 | 94.0 | 25.8 | 0.262 | 171.0 | 47.0 | 0.484 | 316.0 | 86.7 | 0.711 | 464.1 | 127.4 | 1.00 | 652.8 | 179.2 | 1.952 | 1274.3 | 349.8 |
| 1 | WASON | 1662.35 | UNDEV_AG | 873 | 1665.48 | 1.00 | 2220 | 810 | 0.144 | 319.7 | 6 | 0.262 | 581.6 | 212.2 | 0.484 | 1074.5 | 392.0 | 0.711 | 1578.4 | 575.9 | 1.00 | 2220.0 | 810.0 | 1.952 | 4333.4 | 1581.1 |
| 2 | CLARK | 35.05 | URBAN | 888 | 309.20 | 0.11 | 815 | 177 | 0.330 | 29.6 | 6.4 | 0.464 | 41.6 | 9.0 | 0.660 | 59.2 | 12.9 | 0.822 | 73.7 | 16.0 | 1.00 | 89.7 | 19.5 | 1.502 | 134.7 | 29.2 |
| 3 | SUDDEN | 45.07 | UNDEV_AG | 983 | 180.68 | 0.25 | 347 | 106 | 0.144 | 12.5 | 3.8 | 0.262 | 22.7 | 6.9 | 0.484 | 42.0 | 12.8 | 0.711 | 61.7 | 18.8 | 1.00 | 86.8 | 26.5 | 1.952 | 169.3 | 51.7 |
| 4 | BROWN | 30.58 | UNDEV_AG | 980 | 698.76 | 0.04 | 1420 | 402 | 0.144 | 8.2 | 2.3 | 0.262 | 14.9 | 4.2 | 0.484 | 27.5 | 7.8 | 0.711 | 40.4 | 11.4 | 1.00 | 56.8 | 16.1 | 1.952 | 110.9 | 31.4 |
| 5 | WASON | 58.96 | UNDEV_AG | 875 | 199.79 | 0.30 | 397 | 115 | 0.144 | 17.2 | 5.0 | 0.262 | 31.2 | 9.0 | 0.484 | 57.6 | 16.7 | 0.711 | 84.7 | 24.5 | 1.00 | 119.1 | 34.5 | 1.952 | 232.5 | 67.3 |
| 6 | FRANKLIN | 39.54 | UNDEV_AG | 872 | 436.99 | 0.09 | 888 | 253 | 0.144 | 11.5 | 3.3 | 0.262 | 20.9 | 6.0 | 0.484 | 38.7 | 11.0 | 0.711 | 56.8 | 16.2 | 1.00 | 79.9 | 22.8 | 1.952 | 156.0 | 44.4 |
| 7 | SUDDEN | 219.82 | UNDEV_AG | 884 | 231.71 | 0.95 | 372 | 113 | 0.144 | 50.9 | 15.5 | 0.262 | 92.6 | 28.1 | 0.484 | 171.1 | 52.0 | 0.711 | 251.3 | 76.3 | 1.00 | 353.4 | 107.4 | 1.952 | 689.8 | 209.5 |
| 8 | CLARK | 19.55 | URBAN | 889 | 232.70 | 0.08 | 703 | 132 | 0.330 | 18.6 | 3.5 | 0.464 | 26.1 | 4.9 | 0.660 | 37.1 | 7.0 | 0.822 | 46.2 | 8.7 | 1.00 | 56.2 | 10.6 | 1.502 | 84.5 | 15.9 |
| 9 | CLARK | 46.54 | URBAN | 887 | 175.38 | 0.27 | 535 | 99 | 0.330 | 47.7 | 8.8 | 0.464 | 67.0 | 12.4 | 0.660 | 95.3 | 17.6 | 0.822 | 118.7 | 22.0 | 1.00 | 144.5 | 26.7 | 1.502 | 217.0 | 40.1 |
| 10 | CLARK | 31.08 | URBAN | 886 | 93.66 | 0.33 | 274 | 53 | 0.330 | 29.8 | 5.8 | 0.464 | 42.0 | 8.1 | 0.660 | 59.7 | 11.5 | 0.822 | 74.3 | 14.4 | 1.00 | 90.4 | 17.5 | 1.502 | 135.8 | 26.3 |
| 11 | SUDDEN | 36.29 | URBAN | 885 | 109.04 | 0.33 | 299 | 62 | 0.330 | 32.6 | 6.8 | 0.464 | 45.8 | 9.5 | 0.660 | 65.1 | 13.5 | 0.822 | 81.1 | 16.8 | 1.00 | 98.7 | 20.5 | 1.502 | 148.2 | 30.7 |
| 12 | SUDDEN | 22.67 | URBAN | 984 | 165.94 | 0.14 | 489 | 94 | 0.330 | 22.6 | 4.3 | 0.464 | 31.8 | 6.1 | 0.660 | 45.2 | 8.7 | 0.822 | 56.3 | 10.8 | 1.00 | 68.5 | 13.2 | 1.502 | 102.8 | 19.8 |
| 13 | BROWN | 824.08 | UNDEV_AG | 978 | 1005.98 | 0.82 | 1590 | 512 | 0.144 | 187.8 | 60.5 | 0.262 | 341.6 | 110.0 | 0.484 | 631.0 | 203.2 | 0.711 | 927.0 | 298.5 | 1.00 | 1303.8 | 419.8 | 1.952 | 2545.0 | 819.5 |
| 14 | BROWN | 39.27 | URBAN | 979 | 145.53 | 0.27 | 365 | 80 | 0.330 | 32.5 | 7.1 | 0.464 | 45.7 | 10.0 | 0.660 | 65.0 | 14.3 | 0.822 | 81.0 | 17.8 | 1.00 | 98.6 | 21.6 | 1.502 | 148.0 | 32.4 |
| 15 | BROWN | 47.98 | URBAN | 882 | 90.48 | 0.53 | 265 | 51 | 0.330 | 46.4 | 8.9 | 0.464 | 65.2 | 12.5 | 0.660 | 92.7 | 17.8 | 0.822 | 115.5 | 22.2 | 1.00 | 140.5 | 27.0 | 1.502 | 211.0 | 40.6 |
| 16 | SATICOY DRN | 34.98 | URBAN | 876 | 259.13 | 0.13 | 579 | 146 | 0.330 | 24.8 | 6.3 | 0.464 | 34.9 | 8.8 | 0.660 | 49.7 | 12.5 | 0.822 | 61.9 | 15.6 | 1.00 | 75.3 | 19.0 | 1.502 | 113.1 | 28.5 |
| 17 | BROWN | 28.45 | UNDEV_AG | 981 | 183.62 | 0.15 | 433 | 101 | 0.144 | 9.4 | 2.2 | 0.262 | 17.0 | 4.0 | 0.484 | 31.4 | 7.3 | 0.711 | 46.2 | 10.8 | 1.00 | 65.0 | 15.2 | 1.952 | 126.8 | 29.6 |
| 18 | SATICOY YD | 36.12 | URBAN | 878 | 117.61 | 0.31 | 392 | 65 | 0.330 | 40.1 | 6.6 | 0.464 | 56.3 | 9.3 | 0.660 | 80.1 | 13.3 | 0.822 | 99.8 | 16.6 | 1.00 | 121.4 | 20.2 | 1.502 | 182.3 | 30.3 |
| 19 | SCR- | 40.01 | URBAN | 879 | 232.20 | 0.17 | 566 | 127 | 0.330 | 31.7 | 7.1 | 0.464 | 44.6 | 10.0 | 0.660 | 63.5 | 14.2 | 0.822 | 79.1 | 17.7 | 1.00 | 96.2 | 21.6 | 1.502 | 144.5 | 32.4 |
| 20 | SCR- | 26.04 | URBAN | 877 | 76.64 | 0.34 | 202 | 43 | 0.330 | 22.7 | 4.8 | 0.464 | 31.9 | 6.8 | 0.660 | 45.3 | 9.6 | 0.822 | 56.4 | 12.0 | 1.00 | 68.6 | 14.6 | 1.502 | 103.1 | 22.0 |
| 21 | CLARK | 41.20 | UNDEV_AG | 884 | 231.71 | 0.18 | 372 | 113 | 0.144 | 9.6 | 2.9 | 0.262 | 17.5 | 5.3 | 0.484 | 32.4 | 9.8 | 0.711 | 47.6 | 14.5 | 1.00 | 67.0 | 20.3 | 1.952 | 130.7 | 39.7 |
| 22 | BROWN | 48.07 | UNDEV_AG | 871 | 539.83 | 0.09 | 1020 | 280 | 0.144 | 13.2 | 3.6 | 0.262 | 24.1 | 6.6 | 0.484 | 44.4 | 12.2 | 0.711 | 65.3 | 17.9 | 1.00 | 91.8 | 25.2 | 1.952 | 179.2 | 49.2 |
| 23 | BROWN | 99.14 | UNDEV_AG | 978 | 1005.98 | 0.10 | 1590 | 512 | 0.144 | 22.9 | 7.4 | 0.262 | 41.7 | 13.4 | 0.484 | 77.0 | 24.8 | 0.711 | 113.1 | 36.4 | 1.00 | 159.0 | 51.2 | 1.952 | 310.4 | 99.9 |
| 24 | FRANKLIN | 67.67 | UNDEV_AG | 872 | 436.99 | 0.15 | 888 | 253 | 0.144 | 19.2 | 5.5 | 0.262 | 34.9 | 9.9 | 0.484 | 64.5 | 18.4 | 0.711 | 94.7 | 27.0 | 1.00 | 133.2 | 38.0 | 1.952 | 260.0 | 74.1 |
| 25 | SUDDEN | 78.87 | UNDEV_AG | 980 | 698.76 | 0.11 | 1420 | 402 | 0.144 | 22.5 | 6.4 | 0.262 | 40.9 | 11.6 | 0.484 | 75.6 | 21.4 | 0.711 | 111.1 | 31.4 | 1.00 | 156.2 | 44.2 | 1.952 | 304.9 | 86.3 |
| 26 | SUDDEN | 111.69 | UNDEV_AG | 980 | 698.76 | 0.16 | 1420 | 402 | 0.144 | 32.7 | 9.3 | 0.262 | 59.5 | 16.9 | 0.484 | 110.0 | 31.1 | 0.711 | 161.5 | 45.7 | 1.00 | 227.2 | 64.3 | 1.952 | 443.5 | 125.6 |
| 27 | FRANKLIN | 14.84 | UNDEV_AG | 872 | 436.99 | 0.03 | 888 | 253 | 0.144 | 3.8 | 1.1 | 0.262 | 7.0 | 2.0 | 0.484 | 12.9 | 3.7 | 0.711 | | | | | | | | |

Saticoy Area Design Storm Modeling

| ID | Channel | Area Ac. | Primary Land Use | HSPF ID | HSPF AREA ac. | Subarea Ratio | HSPF PEAK cfs | HSPF VOL af | Ratio 5/100-yr | 5-yr Peak cfs | 5-yr Vol af | Ratio 10/100-yr | 10-yr Peak cfs | 10-yr Vol af | Ratio 25/100-yr | 25-yr Peak cfs | 25-yr Vol af | Ratio 50/100-yr | 50-yr Peak cfs | 50-yr Vol af | Ratio 100/100-yr | 100-yr Peak cfs | 100-yr Vol af | Ratio 500/100-yr | 500-yr Peak cfs | 500-yr Vol af |
|----|---------|----------|------------------|---------|---------------|---------------|---------------|-------------|----------------|---------------|-------------|-----------------|----------------|--------------|-----------------|----------------|--------------|-----------------|----------------|--------------|------------------|-----------------|---------------|------------------|-----------------|---------------|
| 37 | CLARK | 67.29 | URBAN | 889 | 232.70 | 0.29 | 703 | 132 | 0.330 | 67.3 | 12.6 | 0.464 | 94.6 | 17.8 | 0.660 | 134.6 | 25.3 | 0.822 | 167.6 | 31.5 | 1.00 | 203.9 | 38.3 | 1.502 | 306.2 | 57.5 |
| 38 | CLARK | 17.85 | URBAN | 889 | 232.70 | 0.08 | 703 | 132 | 0.330 | 18.6 | 3.5 | 0.464 | 26.1 | 4.9 | 0.660 | 37.1 | 7.0 | 0.822 | 46.2 | 8.7 | 1.00 | 56.2 | 10.6 | 1.502 | 84.5 | 15.9 |
| 39 | CLARK | 21.47 | URBAN | 889 | 232.70 | 0.09 | 703 | 132 | 0.330 | 20.9 | 3.9 | 0.464 | 29.4 | 5.5 | 0.660 | 41.8 | 7.8 | 0.822 | 52.0 | 9.8 | 1.00 | 63.3 | 11.9 | 1.502 | 95.0 | 17.8 |
| 40 | CLARK | 11.93 | URBAN | 889 | 232.70 | 0.05 | 703 | 132 | 0.330 | 11.6 | 2.2 | 0.464 | 16.3 | 3.1 | 0.660 | 23.2 | 4.4 | 0.822 | 28.9 | 5.4 | 1.00 | 35.2 | 6.6 | 1.502 | 52.8 | 9.9 |
| 41 | CLARK | 26.05 | URBAN | 888 | 309.20 | 0.08 | 815 | 177 | 0.330 | 21.5 | 4.7 | 0.464 | 30.3 | 6.6 | 0.660 | 43.0 | 9.3 | 0.822 | 53.6 | 11.6 | 1.00 | 65.2 | 14.2 | 1.502 | 97.9 | 21.3 |
| 42 | CLARK | 27.49 | URBAN | 889 | 232.70 | 0.12 | 703 | 132 | 0.330 | 27.8 | 5.2 | 0.464 | 39.1 | 7.3 | 0.660 | 55.7 | 10.5 | 0.822 | 69.3 | 13.0 | 1.00 | 84.4 | 15.8 | 1.502 | 126.7 | 23.8 |
| 43 | CLARK | 24.60 | URBAN | 889 | 232.70 | 0.11 | 703 | 132 | 0.330 | 25.5 | 4.8 | 0.464 | 35.9 | 6.7 | 0.660 | 51.0 | 9.6 | 0.822 | 63.6 | 11.9 | 1.00 | 77.3 | 14.5 | 1.502 | 116.2 | 21.8 |
| 44 | CLARK | 24.97 | URBAN | 888 | 309.20 | 0.08 | 815 | 177 | 0.330 | 21.5 | 4.7 | 0.464 | 30.3 | 6.6 | 0.660 | 43.0 | 9.3 | 0.822 | 53.6 | 11.6 | 1.00 | 65.2 | 14.2 | 1.502 | 97.9 | 21.3 |
| 45 | SUDDEN | 39.74 | UNDEV_AG | 983 | 180.68 | 0.22 | 347 | 106 | 0.144 | 11.0 | 3.4 | 0.262 | 20.0 | 6.1 | 0.484 | 37.0 | 11.3 | 0.711 | 54.3 | 16.6 | 1.00 | 76.3 | 23.3 | 1.952 | 149.0 | 45.5 |
| 46 | CLARK | 35.01 | URBAN | 889 | 232.70 | 0.15 | 703 | 132 | 0.330 | 34.8 | 6.5 | 0.464 | 48.9 | 9.2 | 0.660 | 69.6 | 13.1 | 0.822 | 86.7 | 16.3 | 1.00 | 105.5 | 19.8 | 1.502 | 158.4 | 29.7 |
| 47 | CLARK | 6.63 | URBAN | 887 | 175.38 | 0.04 | 535 | 99 | 0.330 | 7.1 | 1.3 | 0.464 | 9.9 | 1.8 | 0.660 | 14.1 | 2.6 | 0.822 | 17.6 | 3.3 | 1.00 | 21.4 | 4.0 | 1.502 | 32.1 | 5.9 |
| 48 | CLARK | 6.85 | URBAN | 887 | 175.38 | 0.04 | 535 | 99 | 0.330 | 7.1 | 1.3 | 0.464 | 9.9 | 1.8 | 0.660 | 14.1 | 2.6 | 0.822 | 17.6 | 3.3 | 1.00 | 21.4 | 4.0 | 1.502 | 32.1 | 5.9 |
| 49 | CLARK | 35.28 | URBAN | 888 | 309.20 | 0.11 | 815 | 177 | 0.330 | 29.6 | 6.4 | 0.464 | 41.6 | 9.0 | 0.660 | 59.2 | 12.9 | 0.822 | 73.7 | 16.0 | 1.00 | 89.7 | 19.5 | 1.502 | 134.7 | 29.2 |
| 50 | CLARK | 11.06 | URBAN | 888 | 309.20 | 0.04 | 815 | 177 | 0.330 | 10.8 | 2.3 | 0.464 | 15.1 | 3.3 | 0.660 | 21.5 | 4.7 | 0.822 | 26.8 | 5.8 | 1.00 | 32.6 | 7.1 | 1.502 | 49.0 | 10.6 |
| 51 | CLARK | 47.91 | URBAN | 888 | 309.20 | 0.15 | 815 | 177 | 0.330 | 40.3 | 8.8 | 0.464 | 56.7 | 12.3 | 0.660 | 80.7 | 17.5 | 0.822 | 100.5 | 21.8 | 1.00 | 122.3 | 26.6 | 1.502 | 183.6 | 39.9 |
| 52 | CLARK | 31.16 | UNDEV_AG | 888 | 309.20 | 0.10 | 815 | 177 | 0.144 | 11.7 | 2.5 | 0.262 | 21.4 | 4.6 | 0.484 | 39.5 | 8.6 | 0.711 | 58.0 | 12.6 | 1.00 | 81.5 | 17.7 | 1.952 | 159.1 | 34.6 |
| 53 | SUDDEN | 14.31 | URBAN | 983 | 180.68 | 0.08 | 347 | 106 | 0.330 | 9.2 | 2.8 | 0.464 | 12.9 | 3.9 | 0.660 | 18.3 | 5.6 | 0.822 | 22.8 | 7.0 | 1.00 | 27.8 | 8.5 | 1.502 | 41.7 | 12.7 |
| 54 | SUDDEN | 17.53 | UNDEV_AG | 983 | 180.68 | 0.10 | 347 | 106 | 0.144 | 5.0 | 1.5 | 0.262 | 9.1 | 2.8 | 0.484 | 16.8 | 5.1 | 0.711 | 24.7 | 7.5 | 1.00 | 34.7 | 10.6 | 1.952 | 67.7 | 20.7 |
| 55 | BROWN | 30.86 | UNDEV_AG | 980 | 698.76 | 0.04 | 1420 | 402 | 0.144 | 8.2 | 2.3 | 0.262 | 14.9 | 4.2 | 0.484 | 27.5 | 7.8 | 0.711 | 40.4 | 11.4 | 1.00 | 56.8 | 16.1 | 1.952 | 110.9 | 31.4 |
| 56 | SUDDEN | 30.87 | URBAN | 984 | 165.94 | 0.19 | 489 | 94 | 0.330 | 30.7 | 5.9 | 0.464 | 43.1 | 8.3 | 0.660 | 61.3 | 11.8 | 0.822 | 76.4 | 14.7 | 1.00 | 92.9 | 17.9 | 1.502 | 139.6 | 26.8 |
| 57 | SUDDEN | 30.25 | URBAN | 984 | 165.94 | 0.18 | 489 | 94 | 0.330 | 29.1 | 5.6 | 0.464 | 40.8 | 7.9 | 0.660 | 58.1 | 11.2 | 0.822 | 72.4 | 13.9 | 1.00 | 88.0 | 16.9 | 1.502 | 132.2 | 25.4 |
| 58 | SUDDEN | 26.79 | URBAN | 984 | 165.94 | 0.16 | 489 | 94 | 0.330 | 25.8 | 5.0 | 0.464 | 36.3 | 7.0 | 0.660 | 51.6 | 9.9 | 0.822 | 64.3 | 12.4 | 1.00 | 78.2 | 15.0 | 1.502 | 117.5 | 22.6 |
| 59 | SUDDEN | 16.59 | URBAN | 984 | 165.94 | 0.10 | 489 | 94 | 0.330 | 16.1 | 3.1 | 0.464 | 22.7 | 4.4 | 0.660 | 32.3 | 6.2 | 0.822 | 40.2 | 7.7 | 1.00 | 48.9 | 9.4 | 1.502 | 73.5 | 14.1 |
| 60 | CLARK | 7.42 | URBAN | 888 | 309.20 | 0.02 | 815 | 177 | 0.330 | 5.4 | 1.2 | 0.464 | 7.6 | 1.6 | 0.660 | 10.8 | 2.3 | 0.822 | 13.4 | 2.9 | 1.00 | 16.3 | 3.5 | 1.502 | 24.5 | 5.3 |
| 61 | CLARK | 25.57 | URBAN | 888 | 309.20 | 0.08 | 815 | 177 | 0.330 | 21.5 | 4.7 | 0.464 | 30.3 | 6.6 | 0.660 | 43.0 | 9.3 | 0.822 | 53.6 | 11.6 | 1.00 | 65.2 | 14.2 | 1.502 | 97.9 | 21.3 |
| 62 | SUDDEN | 33.10 | UNDEV_AG | 983 | 180.68 | 0.18 | 347 | 106 | 0.144 | 9.0 | 2.7 | 0.262 | 16.4 | 5.0 | 0.484 | 30.2 | 9.2 | 0.711 | 44.4 | 13.6 | 1.00 | 62.5 | 19.1 | 1.952 | 121.9 | 37.2 |
| 63 | BROWN | 30.14 | UNDEV_AG | 980 | 698.76 | 0.04 | 1420 | 402 | 0.144 | 8.2 | 2.3 | 0.262 | 14.9 | 4.2 | 0.484 | 27.5 | 7.8 | 0.711 | 40.4 | 11.4 | 1.00 | 56.8 | 16.1 | 1.952 | 110.9 | 31.4 |
| 64 | BROWN | 35.36 | UNDEV_AG | 980 | 698.76 | 0.05 | 1420 | 402 | 0.144 | 10.2 | 2.9 | 0.262 | 18.6 | 5.3 | 0.484 | 34.4 | 9.7 | 0.711 | 50.5 | 14.3 | 1.00 | 71.0 | 20.1 | 1.952 | 138.6 | 39.2 |
| 65 | BROWN | 25.40 | UNDEV_AG | 980 | | | | | | | | | | | | | | | | | | | | | | |

Saticoy Area Design Storm Modeling

| ID | Channel | Area Ac. | Primary Land Use | HSPF ID | HSPF AREA ac. | Subarea Ratio | HSPF PEAK cfs | HSPF VOL af | Ratio 5/100-yr | 5-yr Peak cfs | 5-yr Vol af | Ratio 10/100-yr | 10-yr Peak cfs | 10-yr Vol af | Ratio 25/100-yr | 25-yr Peak cfs | 25-yr Vol af | Ratio 50/100-yr | 50-yr Peak cfs | 50-yr Vol af | Ratio 100/100-yr | 100-yr Peak cfs | 100-yr Vol af | Ratio 500/100-yr | 500-yr Peak cfs | 500-yr Vol af |
|-----|-------------|----------|------------------|---------|---------------|---------------|---------------|-------------|----------------|---------------|-------------|-----------------|----------------|--------------|-----------------|----------------|--------------|-----------------|----------------|--------------|------------------|-----------------|---------------|------------------|-----------------|---------------|
| 75 | BROWN | 7.75 | URBAN | 981 | 183.62 | 0.04 | 433 | 101 | 0.330 | 5.7 | 1.3 | 0.464 | 8.0 | 1.9 | 0.660 | 11.4 | 2.7 | 0.822 | 14.2 | 3.3 | 1.00 | 17.3 | 4.0 | 1.502 | 26.0 | 6.1 |
| 76 | BROWN | 34.27 | URBAN | 878 | 117.61 | 0.29 | 392 | 65 | 0.330 | 37.5 | 6.2 | 0.464 | 52.7 | 8.7 | 0.660 | 74.9 | 12.4 | 0.822 | 93.3 | 15.5 | 1.00 | 113.5 | 18.9 | 1.502 | 170.5 | 28.3 |
| 77 | BROWN | 42.50 | URBAN | 882 | 90.48 | 0.47 | 265 | 51 | 0.330 | 41.1 | 7.9 | 0.464 | 57.8 | 11.1 | 0.660 | 82.2 | 15.8 | 0.822 | 102.4 | 19.7 | 1.00 | 124.6 | 24.0 | 1.502 | 187.1 | 36.0 |
| 78 | SATICOY DRN | 33.64 | URBAN | 876 | 259.13 | 0.13 | 579 | 146 | 0.330 | 24.8 | 6.3 | 0.464 | 34.9 | 8.8 | 0.660 | 49.7 | 12.5 | 0.822 | 61.9 | 15.6 | 1.00 | 75.3 | 19.0 | 1.502 | 113.1 | 28.5 |
| 79 | FRANKLIN | 24.22 | URBAN | 872 | 436.99 | 0.06 | 888 | 253 | 0.330 | 17.6 | 5.0 | 0.464 | 24.7 | 7.0 | 0.660 | 35.2 | 10.0 | 0.822 | 43.8 | 12.5 | 1.00 | 53.3 | 15.2 | 1.502 | 80.0 | 22.8 |
| 80 | FRANKLIN | 46.29 | UNDEV_AG | 872 | 436.99 | 0.11 | 888 | 253 | 0.144 | 14.1 | 4.0 | 0.262 | 25.6 | 7.3 | 0.484 | 47.3 | 13.5 | 0.711 | 69.5 | 19.8 | 1.00 | 97.7 | 27.8 | 1.952 | 190.7 | 54.3 |
| 81 | FRANKLIN | 48.64 | UNDEV_AG | 872 | 436.99 | 0.11 | 888 | 253 | 0.144 | 14.1 | 4.0 | 0.262 | 25.6 | 7.3 | 0.484 | 47.3 | 13.5 | 0.711 | 69.5 | 19.8 | 1.00 | 97.7 | 27.8 | 1.952 | 190.7 | 54.3 |
| 82 | WASON | 28.14 | UNDEV_AG | 875 | 199.79 | 0.14 | 397 | 115 | 0.144 | 8.0 | 2.3 | 0.262 | 14.6 | 4.2 | 0.484 | 26.9 | 7.8 | 0.711 | 39.5 | 11.4 | 1.00 | 55.6 | 16.1 | 1.952 | 108.5 | 31.4 |
| 83 | CLARK | 26.34 | URBAN | 887 | 175.38 | 0.15 | 535 | 99 | 0.330 | 26.5 | 4.9 | 0.464 | 37.2 | 6.9 | 0.660 | 53.0 | 9.8 | 0.822 | 66.0 | 12.2 | 1.00 | 80.3 | 14.9 | 1.502 | 120.5 | 22.3 |
| 84 | CLARK | 21.22 | URBAN | 887 | 175.38 | 0.12 | 535 | 99 | 0.330 | 21.2 | 3.9 | 0.464 | 29.8 | 5.5 | 0.660 | 42.4 | 7.8 | 0.822 | 52.8 | 9.8 | 1.00 | 64.2 | 11.9 | 1.502 | 96.4 | 17.8 |
| 85 | SUDDEN | 17.41 | URBAN | 984 | 165.94 | 0.10 | 489 | 94 | 0.330 | 16.1 | 3.1 | 0.464 | 22.7 | 4.4 | 0.660 | 32.3 | 6.2 | 0.822 | 40.2 | 7.7 | 1.00 | 48.9 | 9.4 | 1.502 | 73.5 | 14.1 |
| 86 | CLARK | 40.40 | URBAN | 887 | 175.38 | 0.23 | 535 | 99 | 0.330 | 40.6 | 7.5 | 0.464 | 57.1 | 10.6 | 0.660 | 81.2 | 15.0 | 0.822 | 101.2 | 18.7 | 1.00 | 123.1 | 22.8 | 1.502 | 184.8 | 34.2 |
| 87 | CLARK | 21.82 | URBAN | 886 | 93.66 | 0.23 | 274 | 53 | 0.330 | 20.8 | 4.0 | 0.464 | 29.2 | 5.7 | 0.660 | 41.6 | 8.0 | 0.822 | 51.8 | 10.0 | 1.00 | 63.0 | 12.2 | 1.502 | 94.7 | 18.3 |
| 88 | CLARK | 11.57 | URBAN | 886 | 93.66 | 0.12 | 274 | 53 | 0.330 | 10.9 | 2.1 | 0.464 | 15.3 | 3.0 | 0.660 | 21.7 | 4.2 | 0.822 | 27.0 | 5.2 | 1.00 | 32.9 | 6.4 | 1.502 | 49.4 | 9.6 |
| 89 | CLARK | 29.19 | URBAN | 886 | 93.66 | 0.31 | 274 | 53 | 0.330 | 28.0 | 5.4 | 0.464 | 39.4 | 7.6 | 0.660 | 56.1 | 10.8 | 0.822 | 69.8 | 13.5 | 1.00 | 84.9 | 16.4 | 1.502 | 127.6 | 24.7 |
| 90 | CLARK | 13.58 | URBAN | 887 | 175.38 | 0.08 | 535 | 99 | 0.330 | 14.1 | 2.6 | 0.464 | 19.9 | 3.7 | 0.660 | 28.3 | 5.2 | 0.822 | 35.2 | 6.5 | 1.00 | 42.8 | 7.9 | 1.502 | 64.3 | 11.9 |
| 91 | CLARK | 14.25 | URBAN | 887 | 175.38 | 0.08 | 535 | 99 | 0.330 | 14.1 | 2.6 | 0.464 | 19.9 | 3.7 | 0.660 | 28.3 | 5.2 | 0.822 | 35.2 | 6.5 | 1.00 | 42.8 | 7.9 | 1.502 | 64.3 | 11.9 |
| 92 | SCR- | 35.97 | URBAN | 879 | 232.20 | 0.15 | 566 | 127 | 0.330 | 28.0 | 6.3 | 0.464 | 39.4 | 8.8 | 0.660 | 56.0 | 12.6 | 0.822 | 69.8 | 15.7 | 1.00 | 84.9 | 19.1 | 1.502 | 127.5 | 28.6 |
| 93 | SCR- | 40.36 | URBAN | 879 | 232.20 | 0.17 | 566 | 127 | 0.330 | 31.7 | 7.1 | 0.464 | 44.6 | 10.0 | 0.660 | 63.5 | 14.2 | 0.822 | 79.1 | 17.7 | 1.00 | 96.2 | 21.6 | 1.502 | 144.5 | 32.4 |
| 94 | SCR- | 43.77 | URBAN | 885 | 109.04 | 0.40 | 299 | 62 | 0.330 | 39.5 | 8.2 | 0.464 | 55.5 | 11.5 | 0.660 | 78.9 | 16.4 | 0.822 | 98.3 | 20.4 | 1.00 | 119.6 | 24.8 | 1.502 | 179.6 | 37.2 |
| 95 | SCR- | 39.25 | URBAN | 885 | 109.04 | 0.36 | 299 | 62 | 0.330 | 35.5 | 7.4 | 0.464 | 49.9 | 10.4 | 0.660 | 71.0 | 14.7 | 0.822 | 88.5 | 18.3 | 1.00 | 107.6 | 22.3 | 1.502 | 161.7 | 33.5 |
| 96 | SCR- | 60.39 | URBAN | 885 | 109.04 | 0.55 | 299 | 62 | 0.330 | 54.3 | 11.3 | 0.464 | 76.3 | 15.8 | 0.660 | 108.5 | 22.5 | 0.822 | 135.2 | 28.0 | 1.00 | 164.5 | 34.1 | 1.502 | 247.0 | 51.2 |
| 97 | SCR- | 25.35 | URBAN | 885 | 109.04 | 0.23 | 299 | 62 | 0.330 | 22.7 | 4.7 | 0.464 | 31.9 | 6.6 | 0.660 | 45.4 | 9.4 | 0.822 | 56.5 | 11.7 | 1.00 | 68.8 | 14.3 | 1.502 | 103.3 | 21.4 |
| 98 | SCR- | 28.25 | URBAN | 885 | 109.04 | 0.26 | 299 | 62 | 0.330 | 25.7 | 5.3 | 0.464 | 36.1 | 7.5 | 0.660 | 51.3 | 10.6 | 0.822 | 63.9 | 13.3 | 1.00 | 77.7 | 16.1 | 1.502 | 116.8 | 24.2 |
| 99 | SCR- | 19.42 | URBAN | 885 | 109.04 | 0.18 | 299 | 62 | 0.330 | 17.8 | 3.7 | 0.464 | 25.0 | 5.2 | 0.660 | 35.5 | 7.4 | 0.822 | 44.2 | 9.2 | 1.00 | 53.8 | 11.2 | 1.502 | 80.8 | 16.8 |
| 100 | SUDDEN | 23.98 | URBAN | 885 | 109.04 | 0.22 | 299 | 62 | 0.330 | 21.7 | 4.5 | 0.464 | 30.5 | 6.3 | 0.660 | 43.4 | 9.0 | 0.822 | 54.1 | 11.2 | 1.00 | 65.8 | 13.6 | 1.502 | 98.8 | 20.5 |
| 101 | SCR- | 33.84 | URBAN | 885 | 109.04 | 0.31 | 299 | 62 | 0.330 | 30.6 | 6.3 | 0.464 | 43.0 | 8.9 | 0.660 | 61.2 | 12.7 | 0.822 | 76.2 | 15.8 | 1.00 | 92.7 | 19.2 | 1.502 | 139.2 | 28.9 |
| 102 | SCR- | 37.83 | UNDEV_AG | 885 | 109.04 | 0.35 | 299 | 62 | 0.144 | 15.1 | 3.1 | 0.262 | 27.4 | 5.7 | 0.484 | 50.7 | 10.5 | 0.711 | 74.4 | 15.4 | 1.00 | 104.7 | 21.7 | 1.952 | 204.3 | 42.4 |
| 103 | SCR- | 32.78 | | | | | | | | | | | | | | | | | | | | | | | | |

Saticoy Area Design Storm Modeling

| ID | Channel | Area Ac. | Primary Land Use | HSPF ID | HSPF AREA ac. | Subarea Ratio | HSPF PEAK cfs | HSPF VOL af | Ratio 5/100-yr | 5-yr Peak cfs | 5-yr Vol af | Ratio 10/100-yr | 10-yr Peak cfs | 10-yr Vol af | Ratio 25/100-yr | 25-yr Peak cfs | 25-yr Vol af | Ratio 50/100-yr | 50-yr Peak cfs | 50-yr Vol af | Ratio 100/100-yr | 100-yr Peak cfs | 100-yr Vol af | Ratio 500/100-yr | 500-yr Peak cfs | 500-yr Vol af |
|-----|-------------|----------|------------------|---------|---------------|---------------|---------------|-------------|----------------|---------------|-------------|-----------------|----------------|--------------|-----------------|----------------|--------------|-----------------|----------------|--------------|------------------|-----------------|---------------|------------------|-----------------|---------------|
| 114 | SCR- | 16.07 | UNDEV_AG | 885 | 109.04 | 0.15 | 299 | 62 | 0.144 | 6.5 | 1.3 | 0.262 | 11.8 | 2.4 | 0.484 | 21.7 | 4.5 | 0.711 | 31.9 | 6.6 | 1.00 | 44.9 | 9.3 | 1.952 | 87.6 | 18.2 |
| 115 | SCR- | 20.28 | UNDEV_AG | 885 | 109.04 | 0.19 | 299 | 62 | 0.144 | 8.2 | 1.7 | 0.262 | 14.9 | 3.1 | 0.484 | 27.5 | 5.7 | 0.711 | 40.4 | 8.4 | 1.00 | 56.8 | 11.8 | 1.952 | 110.9 | 23.0 |
| 116 | SCR- | 24.18 | URBAN | 885 | 109.04 | 0.22 | 299 | 62 | 0.330 | 21.7 | 4.5 | 0.464 | 30.5 | 6.3 | 0.660 | 43.4 | 9.0 | 0.822 | 54.1 | 11.2 | 1.00 | 65.8 | 13.6 | 1.502 | 98.8 | 20.5 |
| 117 | SCR- | 30.59 | URBAN | 885 | 109.04 | 0.28 | 299 | 62 | 0.330 | 27.6 | 5.7 | 0.464 | 38.9 | 8.1 | 0.660 | 55.3 | 11.5 | 0.822 | 68.8 | 14.3 | 1.00 | 83.7 | 17.4 | 1.502 | 125.8 | 26.1 |
| 118 | SCR- | 32.09 | URBAN | 885 | 109.04 | 0.29 | 299 | 62 | 0.330 | 28.6 | 5.9 | 0.464 | 40.2 | 8.3 | 0.660 | 57.2 | 11.9 | 0.822 | 71.3 | 14.8 | 1.00 | 86.7 | 18.0 | 1.502 | 130.2 | 27.0 |
| 119 | SCR- | 41.52 | URBAN | 885 | 109.04 | 0.38 | 299 | 62 | 0.330 | 37.5 | 7.8 | 0.464 | 52.7 | 10.9 | 0.660 | 75.0 | 15.5 | 0.822 | 93.4 | 19.4 | 1.00 | 113.6 | 23.6 | 1.502 | 170.7 | 35.4 |
| 120 | SCR- | 29.19 | URBAN | 885 | 109.04 | 0.27 | 299 | 62 | 0.330 | 26.6 | 5.5 | 0.464 | 37.5 | 7.8 | 0.660 | 53.3 | 11.0 | 0.822 | 66.4 | 13.8 | 1.00 | 80.7 | 16.7 | 1.502 | 121.3 | 25.1 |
| 121 | SCR- | 37.33 | URBAN | 885 | 109.04 | 0.34 | 299 | 62 | 0.330 | 33.6 | 7.0 | 0.464 | 47.2 | 9.8 | 0.660 | 67.1 | 13.9 | 0.822 | 83.6 | 17.3 | 1.00 | 101.7 | 21.1 | 1.502 | 152.7 | 31.7 |
| 122 | SUDDEN | 21.35 | URBAN | 984 | 165.94 | 0.13 | 489 | 94 | 0.330 | 21.0 | 4.0 | 0.464 | 29.5 | 5.7 | 0.660 | 42.0 | 8.1 | 0.822 | 52.3 | 10.0 | 1.00 | 63.6 | 12.2 | 1.502 | 95.5 | 18.4 |
| 123 | SCR- | 22.26 | URBAN | 885 | 109.04 | 0.20 | 299 | 62 | 0.330 | 19.7 | 4.1 | 0.464 | 27.8 | 5.8 | 0.660 | 39.5 | 8.2 | 0.822 | 49.2 | 10.2 | 1.00 | 59.8 | 12.4 | 1.502 | 89.8 | 18.6 |
| 124 | SUDDEN | 30.28 | URBAN | 885 | 109.04 | 0.28 | 299 | 62 | 0.330 | 27.6 | 5.7 | 0.464 | 38.9 | 8.1 | 0.660 | 55.3 | 11.5 | 0.822 | 68.8 | 14.3 | 1.00 | 83.7 | 17.4 | 1.502 | 125.8 | 26.1 |
| 125 | SUDDEN | 20.21 | URBAN | 885 | 109.04 | 0.19 | 299 | 62 | 0.330 | 18.8 | 3.9 | 0.464 | 26.4 | 5.5 | 0.660 | 37.5 | 7.8 | 0.822 | 46.7 | 9.7 | 1.00 | 56.8 | 11.8 | 1.502 | 85.3 | 17.7 |
| 126 | FRANKLIN | 26.04 | UNDEV_AG | 874 | 196.73 | 0.13 | 389 | 117 | 0.144 | 7.3 | 2.2 | 0.262 | 13.3 | 4.0 | 0.484 | 24.5 | 7.4 | 0.711 | 36.0 | 10.8 | 1.00 | 50.6 | 15.2 | 1.952 | 98.7 | 29.7 |
| 127 | WASON | 55.34 | UNDEV_AG | 875 | 199.79 | 0.28 | 397 | 115 | 0.144 | 16.0 | 4.6 | 0.262 | 29.1 | 8.4 | 0.484 | 53.8 | 15.6 | 0.711 | 79.0 | 22.9 | 1.00 | 111.2 | 32.2 | 1.952 | 217.0 | 62.9 |
| 128 | WASON | 47.38 | UNDEV_AG | 875 | 199.79 | 0.24 | 397 | 115 | 0.144 | 13.7 | 4.0 | 0.262 | 25.0 | 7.2 | 0.484 | 46.1 | 13.4 | 0.711 | 67.7 | 19.6 | 1.00 | 95.3 | 27.6 | 1.952 | 186.0 | 53.9 |
| 129 | FRANKLIN | 40.78 | UNDEV_AG | 874 | 196.73 | 0.21 | 389 | 117 | 0.144 | 11.8 | 3.5 | 0.262 | 21.4 | 6.4 | 0.484 | 39.5 | 11.9 | 0.711 | 58.1 | 17.5 | 1.00 | 81.7 | 24.6 | 1.952 | 159.5 | 48.0 |
| 130 | FRANKLIN | 45.12 | UNDEV_AG | 874 | 196.73 | 0.23 | 389 | 117 | 0.144 | 12.9 | 3.9 | 0.262 | 23.4 | 7.1 | 0.484 | 43.3 | 13.0 | 0.711 | 63.6 | 19.1 | 1.00 | 89.5 | 26.9 | 1.952 | 174.7 | 52.5 |
| 131 | FRANKLIN | 57.14 | UNDEV_AG | 874 | 196.73 | 0.29 | 389 | 117 | 0.144 | 16.2 | 4.9 | 0.262 | 29.6 | 8.9 | 0.484 | 54.6 | 16.4 | 0.711 | 80.2 | 24.1 | 1.00 | 112.8 | 33.9 | 1.952 | 220.2 | 66.2 |
| 132 | FRANKLIN | 29.92 | UNDEV_AG | 874 | 196.73 | 0.15 | 389 | 117 | 0.144 | 8.4 | 2.5 | 0.262 | 15.3 | 4.6 | 0.484 | 28.2 | 8.5 | 0.711 | 41.5 | 12.5 | 1.00 | 58.4 | 17.6 | 1.952 | 113.9 | 34.3 |
| 133 | FRANKLIN | 32.61 | UNDEV_AG | 874 | 196.73 | 0.17 | 389 | 117 | 0.144 | 9.5 | 2.9 | 0.262 | 17.3 | 5.2 | 0.484 | 32.0 | 9.6 | 0.711 | 47.0 | 14.1 | 1.00 | 66.1 | 19.9 | 1.952 | 129.1 | 38.8 |
| 134 | FRANKLIN | 22.58 | UNDEV_AG | 874 | 196.73 | 0.11 | 389 | 117 | 0.144 | 6.2 | 1.9 | 0.262 | 11.2 | 3.4 | 0.484 | 20.7 | 6.2 | 0.711 | 30.4 | 9.2 | 1.00 | 42.8 | 12.9 | 1.952 | 83.5 | 25.1 |
| 135 | FRANKLIN | 32.60 | UNDEV_AG | 874 | 196.73 | 0.17 | 389 | 117 | 0.144 | 9.5 | 2.9 | 0.262 | 17.3 | 5.2 | 0.484 | 32.0 | 9.6 | 0.711 | 47.0 | 14.1 | 1.00 | 66.1 | 19.9 | 1.952 | 129.1 | 38.8 |
| 136 | FRANKLIN | 12.03 | UNDEV_AG | 874 | 196.73 | 0.06 | 389 | 117 | 0.144 | 3.4 | 1.0 | 0.262 | 6.1 | 1.8 | 0.484 | 11.3 | 3.4 | 0.711 | 16.6 | 5.0 | 1.00 | 23.3 | 7.0 | 1.952 | 45.6 | 13.7 |
| 137 | SATICOY YD | 20.26 | URBAN | 878 | 117.61 | 0.17 | 392 | 65 | 0.330 | 22.0 | 3.6 | 0.464 | 30.9 | 5.1 | 0.660 | 43.9 | 7.3 | 0.822 | 54.7 | 9.1 | 1.00 | 66.6 | 11.1 | 1.502 | 100.0 | 16.6 |
| 138 | SATICOY YD | 23.25 | URBAN | 878 | 117.61 | 0.20 | 392 | 65 | 0.330 | 25.8 | 4.3 | 0.464 | 36.3 | 6.0 | 0.660 | 51.7 | 8.6 | 0.822 | 64.4 | 10.7 | 1.00 | 78.3 | 13.0 | 1.502 | 117.6 | 19.5 |
| 139 | SATICOY YD | 10.36 | UNDEV_AG | 885 | 109.04 | 0.10 | 299 | 62 | 0.144 | 4.3 | 0.9 | 0.262 | 7.8 | 1.6 | 0.484 | 14.5 | 3.0 | 0.711 | 21.3 | 4.4 | 1.00 | 29.9 | 6.2 | 1.952 | 58.4 | 12.1 |
| 140 | FRANKLIN | 45.28 | UNDEV_AG | 871 | 539.83 | 0.08 | 1020 | 280 | 0.144 | 11.8 | 3.2 | 0.262 | 21.4 | 5.9 | 0.484 | 39.5 | 10.8 | 0.711 | 58.0 | 15.9 | 1.00 | 81.6 | 22.4 | 1.952 | 159.3 | 43.7 |
| 141 | SATICOY DRN | 16.69 | URBAN | 876 | 259.13 | 0.06 | 579 | 146 | 0.330 | 11.5 | 2.9 | 0.464 | 16.1 | 4.1 | 0.660 | 22.9 | 5.8 | 0.822 | 28.6 | 7.2 | 1.00 | 34.7 | 8.8 | 1.502 | 52.2 | 13. |

Saticoy Area Design Storm Modeling

| ID | Channel | Area Ac. | Primary Land Use | HSPF ID | HSPF AREA ac. | Subarea Ratio | HSPF PEAK cfs | HSPF VOL af | Ratio 5/100-yr | 5-yr Peak cfs | 5-yr Vol af | Ratio 10/100-yr | 10-yr Peak cfs | 10-yr Vol af | Ratio 25/100-yr | 25-yr Peak cfs | 25-yr Vol af | Ratio 50/100-yr | 50-yr Peak cfs | 50-yr Vol af | Ratio 100/100-yr | 100-yr Peak cfs | 100-yr Vol af | Ratio 500/100-yr | 500-yr Peak cfs | 500-yr Vol af |
|-----|-------------|----------|------------------|---------|---------------|---------------|---------------|-------------|----------------|---------------|-------------|-----------------|----------------|--------------|-----------------|----------------|--------------|-----------------|----------------|--------------|------------------|-----------------|---------------|------------------|-----------------|---------------|
| 152 | SCR- | 20.27 | UNDEV_AG | 885 | 109.04 | 0.19 | 299 | 62 | 0.144 | 8.2 | 1.7 | 0.262 | 14.9 | 3.1 | 0.484 | 27.5 | 5.7 | 0.711 | 40.4 | 8.4 | 1.00 | 56.8 | 11.8 | 1.952 | 110.9 | 23.0 |
| 153 | FRANKLIN | 28.81 | UNDEV_AG | 872 | 436.99 | 0.07 | 888 | 253 | 0.144 | 9.0 | 2.6 | 0.262 | 16.3 | 4.6 | 0.484 | 30.1 | 8.6 | 0.711 | 44.2 | 12.6 | 1.00 | 62.2 | 17.7 | 1.952 | 121.3 | 34.6 |
| 154 | FRANKLIN | 15.81 | UNDEV_AG | 872 | 436.99 | 0.04 | 888 | 253 | 0.144 | 5.1 | 1.5 | 0.262 | 9.3 | 2.7 | 0.484 | 17.2 | 4.9 | 0.711 | 25.3 | 7.2 | 1.00 | 35.5 | 10.1 | 1.952 | 69.3 | 19.8 |
| 155 | FRANKLIN | 17.93 | UNDEV_AG | 872 | 436.99 | 0.04 | 888 | 253 | 0.144 | 5.1 | 1.5 | 0.262 | 9.3 | 2.7 | 0.484 | 17.2 | 4.9 | 0.711 | 25.3 | 7.2 | 1.00 | 35.5 | 10.1 | 1.952 | 69.3 | 19.8 |
| 156 | FRANKLIN | 25.06 | UNDEV_AG | 872 | 436.99 | 0.06 | 888 | 253 | 0.144 | 7.7 | 2.2 | 0.262 | 14.0 | 4.0 | 0.484 | 25.8 | 7.3 | 0.711 | 37.9 | 10.8 | 1.00 | 53.3 | 15.2 | 1.952 | 104.0 | 29.6 |
| 157 | FRANKLIN | 34.14 | UNDEV_AG | 876 | 259.13 | 0.13 | 579 | 146 | 0.144 | 10.8 | 2.7 | 0.262 | 19.7 | 5.0 | 0.484 | 36.4 | 9.2 | 0.711 | 53.5 | 13.5 | 1.00 | 75.3 | 19.0 | 1.952 | 146.9 | 37.0 |
| 158 | FRANKLIN | 25.02 | UNDEV_AG | 876 | 259.13 | 0.10 | 579 | 146 | 0.144 | 8.3 | 2.1 | 0.262 | 15.2 | 3.8 | 0.484 | 28.0 | 7.1 | 0.711 | 41.2 | 10.4 | 1.00 | 57.9 | 14.6 | 1.952 | 113.0 | 28.5 |
| 159 | FRANKLIN | 26.29 | UNDEV_AG | 872 | 436.99 | 0.06 | 888 | 253 | 0.144 | 7.7 | 2.2 | 0.262 | 14.0 | 4.0 | 0.484 | 25.8 | 7.3 | 0.711 | 37.9 | 10.8 | 1.00 | 53.3 | 15.2 | 1.952 | 104.0 | 29.6 |
| 160 | FRANKLIN | 22.06 | UNDEV_AG | 872 | 436.99 | 0.05 | 888 | 253 | 0.144 | 6.4 | 1.8 | 0.262 | 11.6 | 3.3 | 0.484 | 21.5 | 6.1 | 0.711 | 31.6 | 9.0 | 1.00 | 44.4 | 12.7 | 1.952 | 86.7 | 24.7 |
| 161 | SATICOY DRN | 26.08 | URBAN | 876 | 259.13 | 0.10 | 579 | 146 | 0.330 | 19.1 | 4.8 | 0.464 | 26.9 | 6.8 | 0.660 | 38.2 | 9.6 | 0.822 | 47.6 | 12.0 | 1.00 | 57.9 | 14.6 | 1.502 | 87.0 | 21.9 |
| 162 | BROWN | 26.24 | UNDEV_AG | 980 | 698.76 | 0.04 | 1420 | 402 | 0.144 | 8.2 | 2.3 | 0.262 | 14.9 | 4.2 | 0.484 | 27.5 | 7.8 | 0.711 | 40.4 | 11.4 | 1.00 | 56.8 | 16.1 | 1.952 | 110.9 | 31.4 |
| 163 | BROWN | 25.97 | URBAN | 981 | 183.62 | 0.14 | 433 | 101 | 0.330 | 20.0 | 4.7 | 0.464 | 28.1 | 6.6 | 0.660 | 40.0 | 9.3 | 0.822 | 49.8 | 11.6 | 1.00 | 60.6 | 14.1 | 1.502 | 91.1 | 21.2 |
| 164 | BROWN | 29.76 | URBAN | 981 | 183.62 | 0.16 | 433 | 101 | 0.330 | 22.9 | 5.3 | 0.464 | 32.2 | 7.5 | 0.660 | 45.7 | 10.7 | 0.822 | 57.0 | 13.3 | 1.00 | 69.3 | 16.2 | 1.502 | 104.1 | 24.3 |
| 165 | BROWN | 25.24 | URBAN | 981 | 183.62 | 0.14 | 433 | 101 | 0.330 | 20.0 | 4.7 | 0.464 | 28.1 | 6.6 | 0.660 | 40.0 | 9.3 | 0.822 | 49.8 | 11.6 | 1.00 | 60.6 | 14.1 | 1.502 | 91.1 | 21.2 |
| 166 | BROWN | 81.35 | UNDEV_AG | 978 | 1005.98 | 0.08 | 1590 | 512 | 0.144 | 18.3 | 5.9 | 0.262 | 33.3 | 10.7 | 0.484 | 61.6 | 19.8 | 0.711 | 90.4 | 29.1 | 1.00 | 127.2 | 41.0 | 1.952 | 248.3 | 80.0 |
| 167 | BROWN | 37.12 | UNDEV_AG | 978 | 1005.98 | 0.04 | 1590 | 512 | 0.144 | 9.2 | 2.9 | 0.262 | 16.7 | 5.4 | 0.484 | 30.8 | 9.9 | 0.711 | 45.2 | 14.6 | 1.00 | 63.6 | 20.5 | 1.952 | 124.2 | 40.0 |
| 168 | SCR- | 59.19 | UNDEV_AG | 874 | 196.73 | 0.30 | 389 | 117 | 0.144 | 16.8 | 5.1 | 0.262 | 30.6 | 9.2 | 0.484 | 56.5 | 17.0 | 0.711 | 83.0 | 25.0 | 1.00 | 116.7 | 35.1 | 1.952 | 227.8 | 68.5 |
| 169 | SCR- | 48.26 | UNDEV_AG | 874 | 196.73 | 0.25 | 389 | 117 | 0.144 | 14.0 | 4.2 | 0.262 | 25.5 | 7.7 | 0.484 | 47.1 | 14.2 | 0.711 | 69.1 | 20.8 | 1.00 | 97.3 | 29.3 | 1.952 | 189.8 | 57.1 |
| 170 | SCR- | 52.66 | UNDEV_AG | 874 | 196.73 | 0.27 | 389 | 117 | 0.144 | 15.1 | 4.5 | 0.262 | 27.5 | 8.3 | 0.484 | 50.8 | 15.3 | 0.711 | 74.7 | 22.5 | 1.00 | 105.0 | 31.6 | 1.952 | 205.0 | 61.7 |
| 171 | CLARK | 27.94 | UNDEV_AG | 888 | 309.20 | 0.09 | 815 | 177 | 0.144 | 10.6 | 2.3 | 0.262 | 19.2 | 4.2 | 0.484 | 35.5 | 7.7 | 0.711 | 52.2 | 11.3 | 1.00 | 73.4 | 15.9 | 1.952 | 143.2 | 31.1 |
| 172 | SUDDEN | 30.78 | UNDEV_AG | 983 | 180.68 | 0.17 | 347 | 106 | 0.144 | 8.5 | 2.6 | 0.262 | 15.5 | 4.7 | 0.484 | 28.6 | 8.7 | 0.711 | 41.9 | 12.8 | 1.00 | 59.0 | 18.0 | 1.952 | 115.2 | 35.2 |
| 173 | BROWN | 29.59 | UNDEV_AG | 980 | 698.76 | 0.04 | 1420 | 402 | 0.144 | 8.2 | 2.3 | 0.262 | 14.9 | 4.2 | 0.484 | 27.5 | 7.8 | 0.711 | 40.4 | 11.4 | 1.00 | 56.8 | 16.1 | 1.952 | 110.9 | 31.4 |
| 174 | BROWN | 28.20 | UNDEV_AG | 980 | 698.76 | 0.04 | 1420 | 402 | 0.144 | 8.2 | 2.3 | 0.262 | 14.9 | 4.2 | 0.484 | 27.5 | 7.8 | 0.711 | 40.4 | 11.4 | 1.00 | 56.8 | 16.1 | 1.952 | 110.9 | 31.4 |
| 175 | BROWN | 26.53 | UNDEV_AG | 980 | 698.76 | 0.04 | 1420 | 402 | 0.144 | 8.2 | 2.3 | 0.262 | 14.9 | 4.2 | 0.484 | 27.5 | 7.8 | 0.711 | 40.4 | 11.4 | 1.00 | 56.8 | 16.1 | 1.952 | 110.9 | 31.4 |
| 176 | BROWN | 22.75 | UNDEV_AG | 980 | 698.76 | 0.03 | 1420 | 402 | 0.144 | 6.1 | 1.7 | 0.262 | 11.2 | 3.2 | 0.484 | 20.6 | 5.8 | 0.711 | 30.3 | 8.6 | 1.00 | 42.6 | 12.1 | 1.952 | 83.2 | 23.5 |
| 177 | CLARK | 19.36 | URBAN | 888 | 309.20 | 0.06 | 815 | 177 | 0.330 | 16.1 | 3.5 | 0.464 | 22.7 | 4.9 | 0.660 | 32.3 | 7.0 | 0.822 | 40.2 | 8.7 | 1.00 | 48.9 | 10.6 | 1.502 | 73.5 | 16.0 |